

Artifact reduction in pseudo-acoustic modeling by pseudo-source injection

SEP 152, pages 95-104

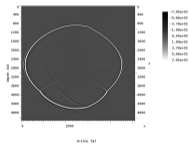
Musa Maharramov

Stanford Exploration Project

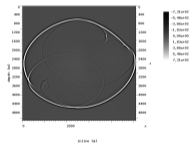
June 4, 2013

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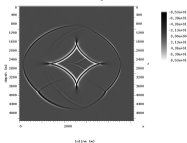
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- Motivation
- Overview of existing pseudo-acoustic methods
- Evolutionary pseudo-differential equation
- **NEW:** *pseudo-sources* and finite-difference systems
- Numerical tests
- Conclusions and perspectives
- Acknowledgements



- Computationally efficient pseudo-acoustic modeling is of significant value for applications (Fowler et al, 2010)
- FD methods are fast but suffer from *pseudo-shear* artifacts (Alkhalifah, 2000; Zhang and Zhang, 2008; Fletcher et al., 2009)
- Artifact-free spectral methods require multiple FFTs per time step (Etgen and Brandsberg-Dahl, 2009)
- **Goal: a fast FD method with a significant reduction of pseudo-shear artifacts**



Convert the azimuthal pressure velocity curve $V(\theta)$ (Tsvankin 2001) into a pseudo-differential equation

$$\begin{aligned} \frac{V^2(\theta)}{V_P^2} &= 1 + \epsilon \sin^2 \theta - \frac{f}{2} \pm \\ &\pm \left\{ \left(1 + \frac{2\epsilon \sin^2 \theta}{f} \right)^2 - \frac{2(\epsilon - \delta) \sin^2 2\theta}{f} \right\}^{1/2}, \end{aligned} \quad (1)$$
$$f = 1 - \frac{V_S^2}{V_P^2}, \quad \sin \theta = \frac{V(\theta) \left[\frac{\partial}{\partial x} \right]}{\left[\frac{\partial}{\partial t} \right]}, \quad \cos \theta = \frac{V(\theta) \left[\frac{\partial}{\partial z} \right]}{\left[\frac{\partial}{\partial t} \right]}$$

and solve it using a spectral method plus interpolation.



The full pseudo-differential operator equation (1) can be approximated with a trigonometric polynomial:

$$V^2(\theta) \approx V_P^2 \sum_{n=0}^N a_n \sin^{2n}(\theta), \quad (2)$$

leading to separable pseudo-differential operators used in practice:

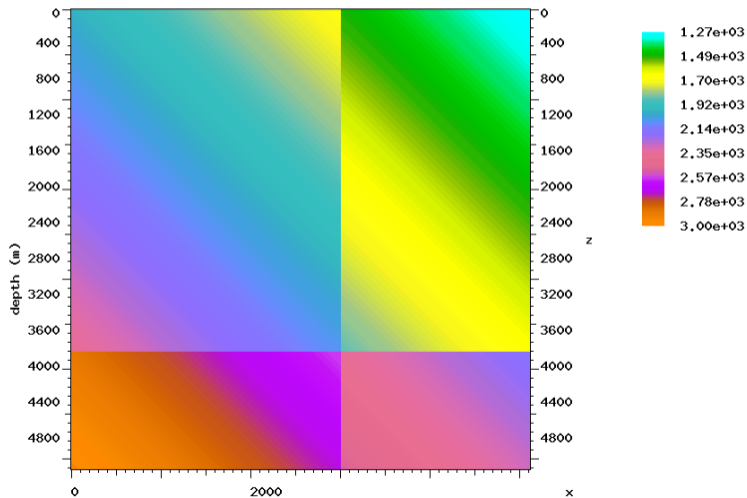
$$\frac{\partial^2}{\partial t^2} = V_P^2 \sum_{n=0}^N a_n \frac{\partial^{2n}}{\partial x^{2n}} \Delta^{1-n}, \quad (3)$$

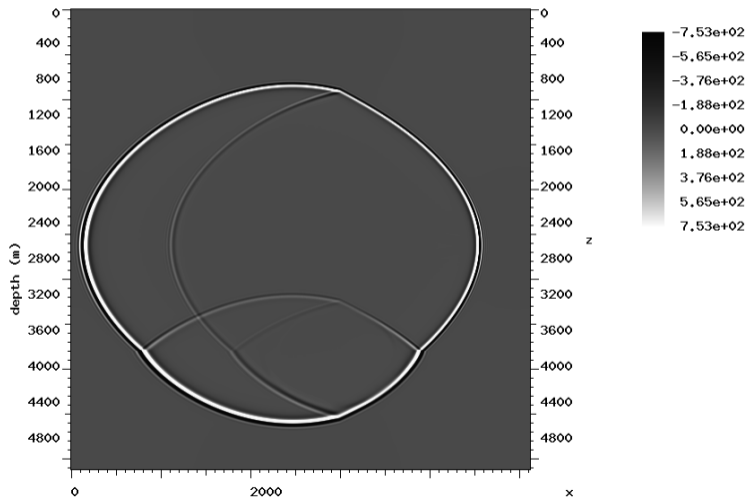
Examples of (2), the *weak anisotropy* approximation:

$$V^2(\theta) \approx V_P^2 \left(1 + \delta \sin^2 \theta + \frac{\epsilon - \delta}{1 + 2\delta} \sin^4 \theta \right), \quad (4)$$

and Harlan and Lazear relation (Etgen and Brandsberg-Dahl, 2009):

$$V^2(\theta) = V_P^2 \cos^2 \theta + (V_{PNMO}^2 - V_{PHor}^2) \cos^2 \theta \sin^2 \theta + V_{PHor}^2 \sin^2 \theta, \quad (5)$$







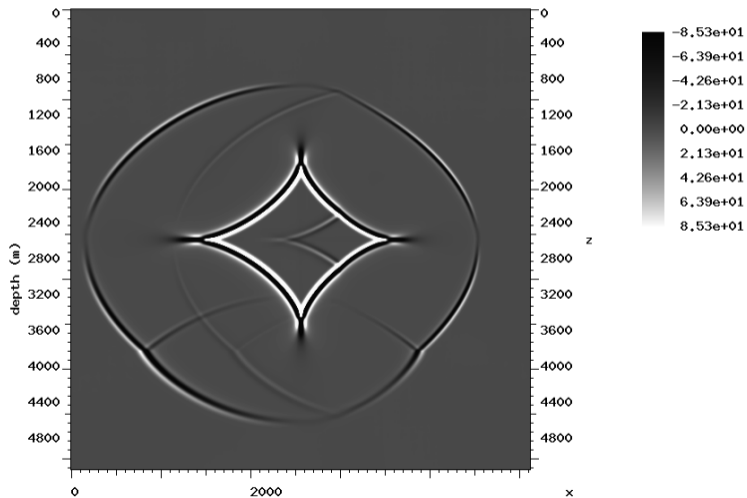
Convert (1) into a DO by squaring the square root (Alkhalifah, 2000):

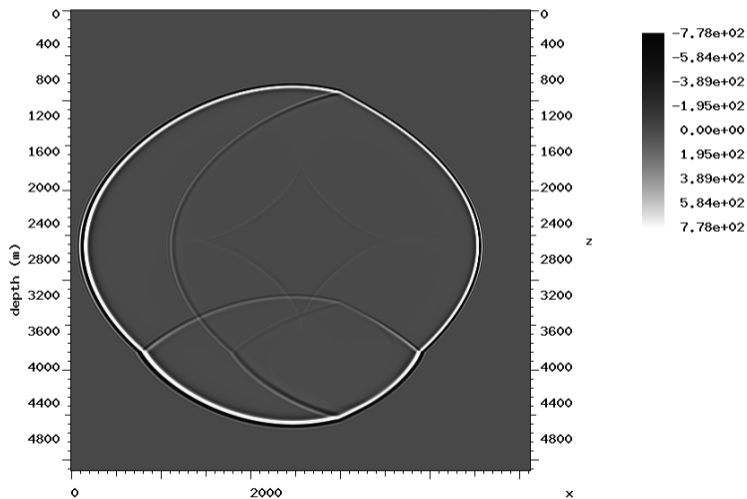
$$\begin{aligned}\frac{\partial^2 q}{\partial t^2} &= V_{P\text{Hor}}^2 \frac{\partial^2 q}{\partial x^2} + V_P^2 \frac{\partial^2 q}{\partial z^2} + V_P^2 (V_{P\text{Hor}}^2 - V_{P\text{NMO}}^2) \frac{\partial^4 r}{\partial x^2 \partial z^2}, \\ \frac{\partial^2 r}{\partial t^2} &= q,\end{aligned}\tag{6}$$

where

$$V_{P\text{Hor}}^2 = V_P^2 (1 + 2\epsilon), \quad V_{P\text{NMO}}^2 = V_P^2 (1 + 2\delta).\tag{7}$$

- r corresponds to solution of (1)
- In *conventional implementations* source is injected in q
- Equivalent systems exist with components as linear combinations of r and q



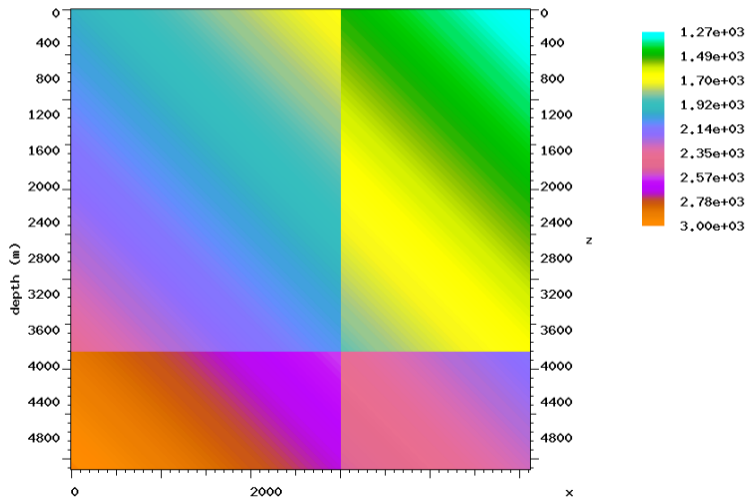


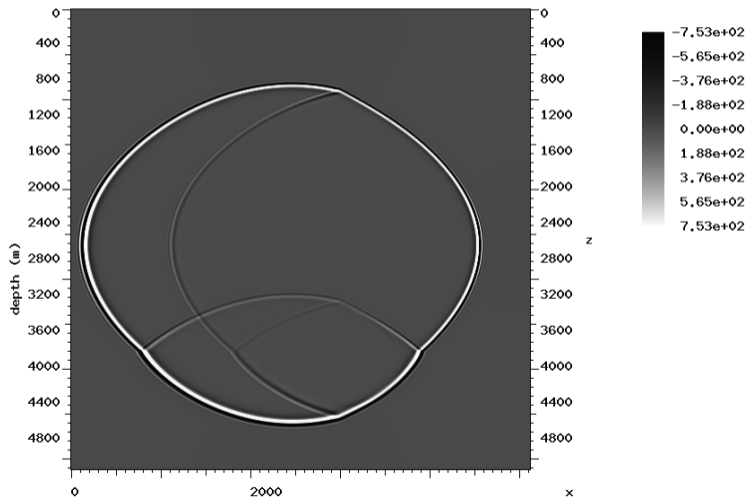


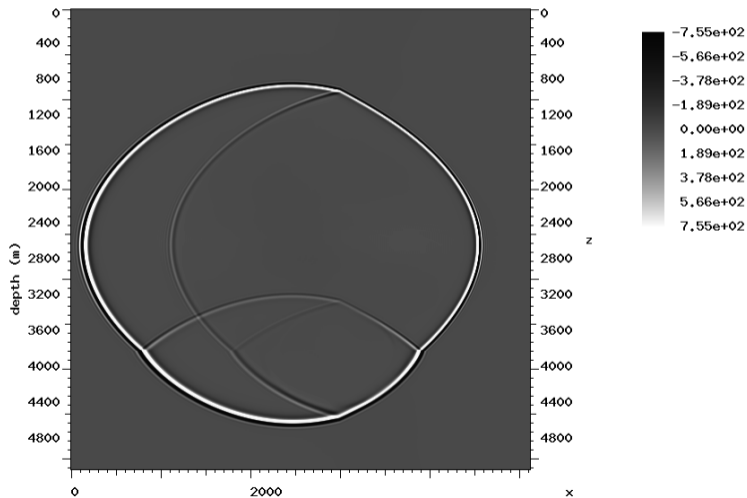
At each time step inject the actual source in r and the *pseudo-source* into q :

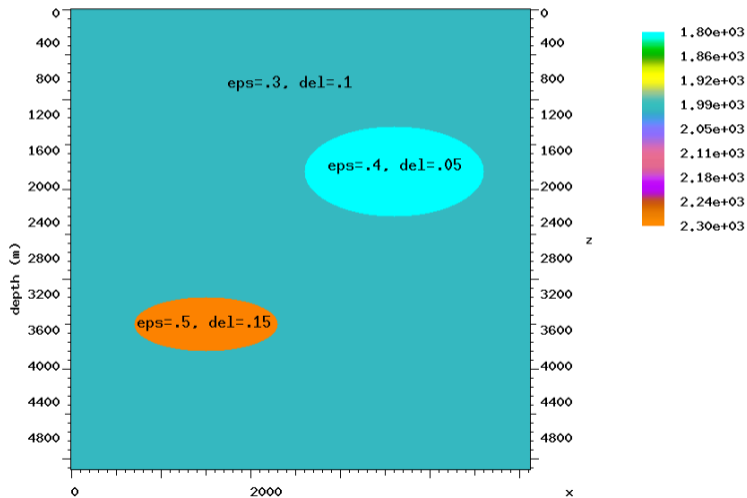
$$\begin{aligned}
 r(z, x, t_n) &= r(z, x, t_n) + \phi(z, x, t_n), \\
 q(z, x, t_n) &= q(z, x, t_n) + V_P^2 \left\{ (z, x) \frac{\Delta}{2} + \epsilon(z, x) \frac{\partial^2}{\partial x^2} + \right. \\
 &\quad \left. + \frac{\Delta}{2} \sqrt{\left[1 + 2\epsilon(z, z) \frac{\partial^2}{\partial x^2} \frac{1}{\Delta} \right]^2 - 8(\epsilon(z, x) - \delta(z, x)) \frac{\partial^2}{\partial x^2} \frac{\partial^2}{\partial z^2} \frac{1}{\Delta^2}} \right\} \phi,
 \end{aligned} \tag{8}$$

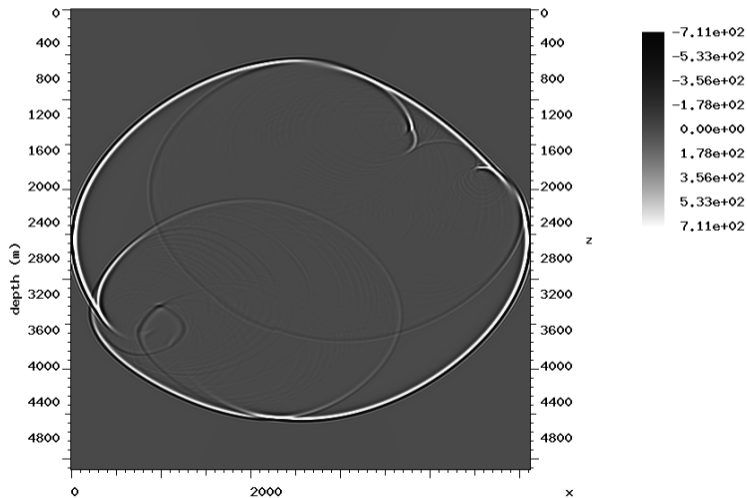
Apply the finite-difference time step of (6).

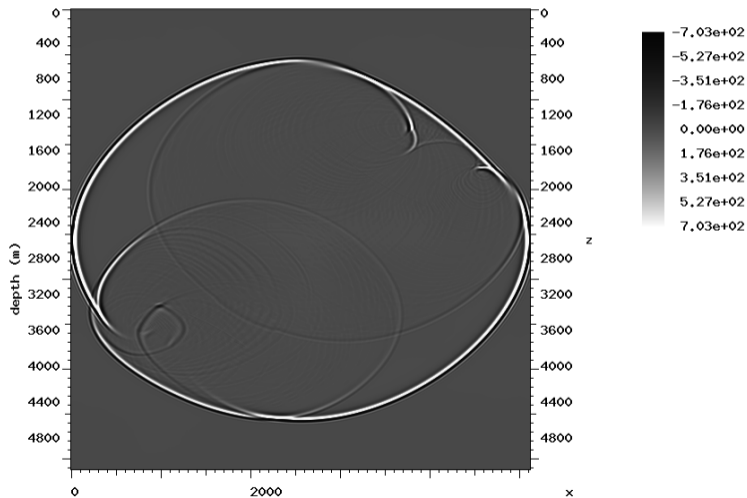


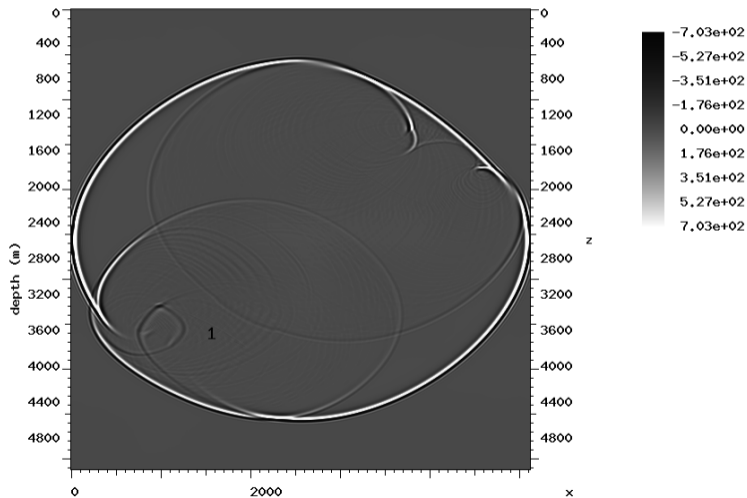




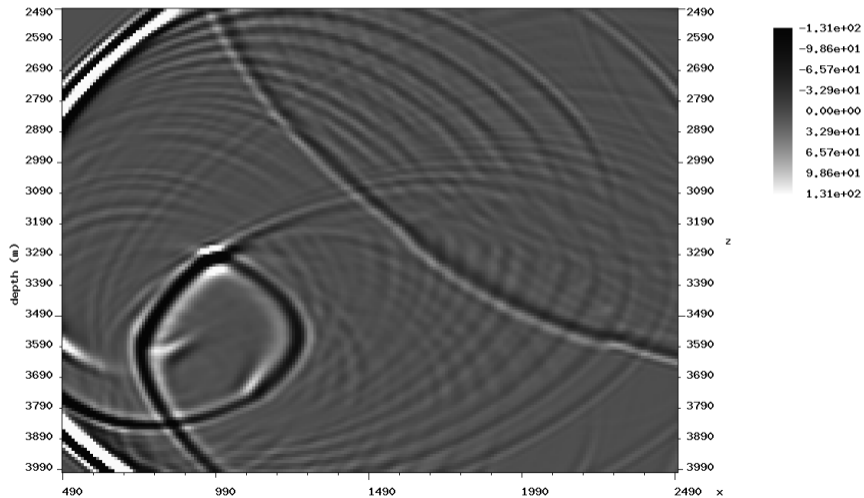


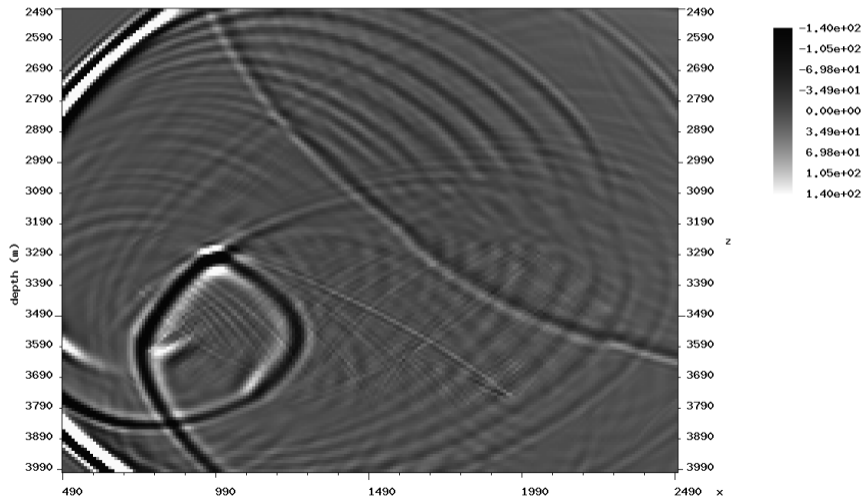




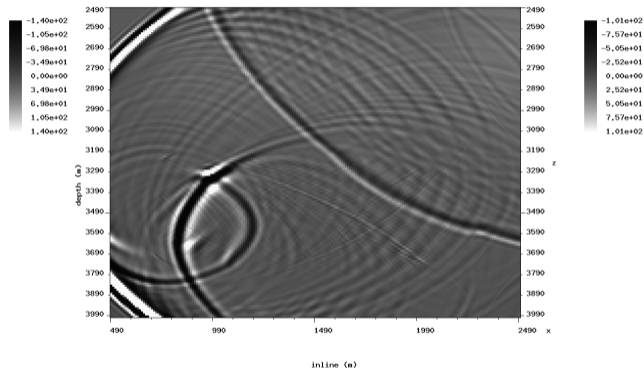
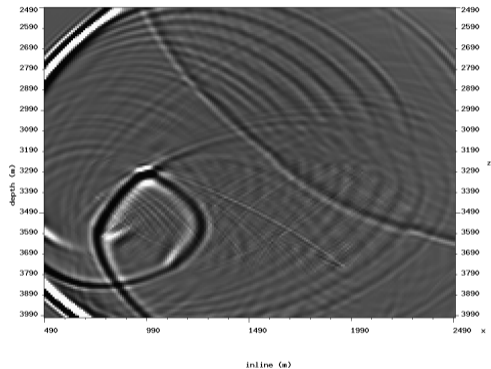


Pseudo-differential operator – ϵ, δ contrasts



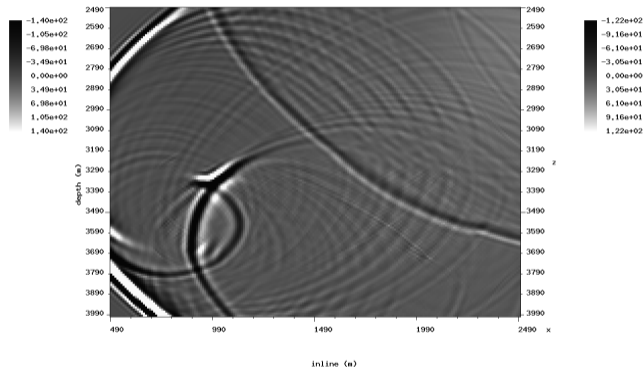
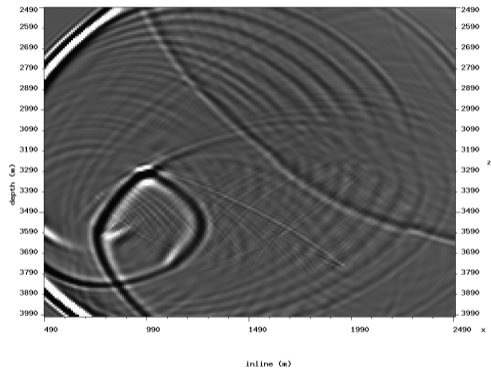


Non-smoothed Thomsen vs smoothed Thomsen



Weak high-frequency artifacts appear where FD approximation has largest errors.

Non-smoothed Thomsen vs constant Thomsen



Reduction in FD error (and error anisotropy) reduces the artifacts.



- Computationally cheap FD technique with artifacts suppressed by injecting a “pseudo-source”
- Savings come from spatial boundedness of pseudo-source support
- Achieves a significant reduction of shear artifacts
- Can be used with a wide range of PA systems (Fowler et al., 2010)
- **Next steps:** apply to energy-conserving tilted anisotropy systems (Zhang and Zhang, 2009; Macesanu, 2011)
- Combine with Lax-Wendroff to reduce dispersion



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